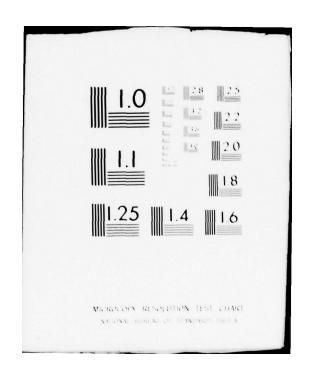
WOODWARD-CLYDE CONSULTANTS PLYMOUTH MEETING PA AD-A072 904 NATIONAL DAM INSPECTION PROGRAM. MINSI DAM (NDS ID PA 00788 DER--ETC(U) JUN 79 DACW31-79-C-0017 UNCLASSIFIED | OF | AD 72904 END DATE FILMED 9-79 DDC



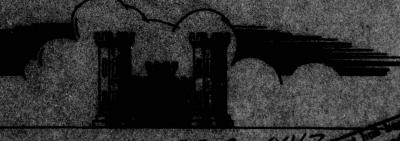
MAC72904

LIME

MINSTIDAM

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

> DRIGHAL CONTAINS COLOR PLAYED: ALL DOC SEPHIODOCTIONS WILL BE M. BEACK AND WHITE



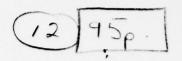
Conteset in DACU31-79-C-00/

BREARTMENT OF THE ARMY Baldiners District, Coups of Engineers Buttleore, Maryland 21203

JUNE 1919

79 08 15 493

National Dem Inspection Program. Minsi Dam (NDS ID PA 00788 DER ID 48-139), Delaware River Basin, East Branch Martin's Creek, Northampton, County, Pennsylvania. Phase I Inspection Report.

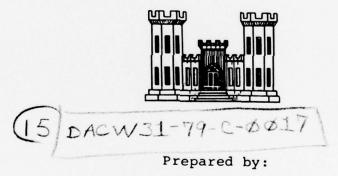


DELAWARE RIVER BASIN

MINSI DAM, NORTHAMPTON COUNTY PENNSYLVANIA

NDS I.D. NO. PA 00788 DER I.D. NO. 48-139

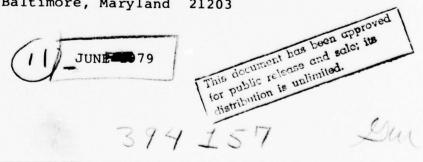
PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM



WOODWARD-CLYDE CONSULTANTS 5120 Butler Pike Plymouth Meeting, Pennsylvania 19462

Submitted to:

DEPARTMENT OF THE ARMY
Baltimore District, Corps of Engineers
Baltimore, Maryland 21203





This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of the Chief of Engineers, Washington, D. C., 20314. The purpose of a Phase I investigation is to expeditiously identify those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify the need for more detailed studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected, and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam: County Located: State Located: Stream:

Minsi Lake Dam Northampton County Pennsylvania

Stream: East Branch Martins Creek
Coordinates: Latitude 40° 54.7'
Longitude 75° 10.3'

Date of Inspection: 19 April 1979

Minsi Lake Dam is owned by the Pennsylvania Fish Commission. Preliminary design drawings were prepared by Jordan, McNee, Parnum & Yule of Camp Hill, Pennsylvania, in 1966, and construction began in July 1969. The facility is considered to be in good condition and well maintained. The dam is classified as a "High" hazard potential structure consistent with its potential, in the event of failure, to cause extensive property damage and possible loss of life downstream. The dam is also classified as an "Intermediate" size dam by virtue of its 1,793 acre-foot total storage capacity.

Design documentation, specifications and the visual inspection provided sufficient information to evaluate the embankment and appurtenant structures in accordance with provisions of the Phase I Inspection program.

Hydrologic and hydraulic calculations presented in Appendix C indicate the dam will pass approximately 70 percent of the Probable Maximum Flood (PMF) without overtopping. Therefore, the spillway system is considered to be "Inadequate" but not "Seriously Inadequate" as it passes more than 50 percent of the PMF.

Visual inspection of the dam and reservoir detected no significant problems other than some wet areas downstream, which were assessed to be associated with adverse drainage downstream. Also, slight deterioration of the upstream embankment facing was noted as a result of wave action and ice forces.

The following recommendations are suggested to insure that the structure is maintained in the best possible condition. All engineering evaluations pertaining to corrective work or the need for corrective work should be reviewed

by a registered professional engineer experienced in the design of dams.

- 1. The marshy area at the toe of the structure should be regraded and drained away from the dam. quently, seepage should be monitored to determine if it flows through the embankment. Should it be determined that seepage flows through the embankment, appropriate remedial measures should be taken to control this flow.
- 2. Concrete block on the upstream slopes should continue to be monitored, especially during the spring of each year. Deteriorated block should be removed and replaced with new block.

Date

OHN BOSCHUN, JE

Operation and maintenance procedures currently in draft form should be issued as soon as possible. The Owner should be sure to develop an operation and maintenance checklist which would be used during the regular inspections to insure that all items of the structure are maintained in the best possible condition.

John Boschuk, Jr., P.E. Pennsylvania Registration 27450E

Woodward-Clyde Consultants

John H. Frederick, Jr., Maryland Registration 7301

Woodward-Clyde Consultants

APPROVED BY:

JAMES W. PECK

Colonel, Corps of Engineers

District Engineer

iii



OVERVIEW MINSI DAM, NORTHAMPTON COUNTY, PENNSYLVANIA

TABLE OF CONTENTS

	PAGE
Preface Assessment and Recommendations Overview Photograph	i ii iv
SECTION 1 - PROJECT INFORMATION 1.1 General 1.2 Description of Project 1.3 Pertinent Data	1 1 4
SECTION 2 - ENGINEERING DATA 2.1 Design 2.2 Construction 2.3 Operational Data 2.4 Evaluation	6 6 6 7
SECTION 3 - VISUAL INSPECTION 3.1 Findings 3.2 Evaluation	8
SECTION 4 - OPERATIONAL PROCEDURES 4.1 Procedures 4.2 Maintenance of the Dam 4.3 Maintenance of Operating Facilities 4.4 Warning Systems In Effect 4.5 Evaluation	10 10 10 10
SECTION 5 - HYDROLOGY/HYDRAULICS 5.1 Evaluation of Features	11
SECTION 6 - STRUCTURAL STABILITY 6.1 Evaluation of Structural Stability	13
SECTION 7 - ASSESSMENT/REMEDIAL MEASURES 7.1 Dam Assessment 7.2 Remedial Measures	15 15
APPENDIX A Engineering Data, Design, Construction and Operation	
B Visual Inspection C Hydrology/Hydraulics D Photographs E Plates	
F Geology	

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM MINSI LAKE DAM NATIONAL ID #PA 00788 DER #48-139

SECTION 1 PROJECT INFORMATION

1.1 General.

- a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

a. Dam and Appurtenances. Minsi Lake Dam is a 26.5 foot high zoned earth embankment across East Branch Martins Creek. The dam has a maximum length of 3,000 feet and the 117-acre reservoir has a normal storage capacity of 960 acre-feet.

The zoned earth embankment contains an impervious core over a 12 foot wide cutoff trench under the centerline of the dam. As shown on Plate 4, the upstream side consists of Class A fill and the slope is 3H:1V. The upstream slope is also protected with hand-placed concrete blocks over a nine-inch crushed stone filter course from elevation 694 to the crest, 703.5. The blocks are 8 by 12 by 16 inches nominal and placed with a 12-inch face exposed. The downstream slope contains a Class B fill beneath a pervious shell. The shell is connected to the toe drain by a filter. The toe drain porous drain pipe discharges into the fish catch basin. The downstream slope is 2.5H:1V and is protected with grass. Typical embankment sections are shown on Plate 4.

The dam was designed by the Pennsylvania Fish Commission and contains a standard Fish Commission intake tower located about 15 feet upstream of the centerline at Station 17 + 65. The tower contains an interior overflow weir formed by stoplogs. Water enters the tower through a 3 foot by 3 foot concrete conduit extending from the upstream toe through the embankment to the intake tower base. A 3 foot by 3

foot concrete discharge conduit extends from the tower to the downstream toe. The entrance invert is at elevation 677.5 and the exit invert is at elevation 677. There are four anti-seep collars, two upstream and two downstream of the tower. The top of the tower is at elevation 706.67, and normal pool elevation corresponds to approximately 698, the crest of the emergency spillway weir. Normal pool elevation is controlled by both the stoplogs within the tower and the emergency spillway. The reservoir drain is through the tower, invert elevation 677.3, and is controlled by a 2 foot by 2 foot sluice gate. The tower also contains a two-inch cast iron minimum flow pipe and valve which are used to maintain minimum flow downstream. Typical section, plan and profile views are enclosed as Plates 6 and 7.

The emergency spillway located at the left abutment consists of a concrete trapezoidal weir at elevation 698.0. The 80 foot wide spillway is shown on Plates 3c and 8 with a typical cross-section on Plates 8 and 9.

- b. Location. Minsi Lake Dam is on East Branch Martins Creek about 2-3/4 miles north of East Bangor, Pennsylvania. The dam and reservoir are located in Upper Mount Bethel Township, Northampton County, Pennsylvania, and are located on the "Stroudsburg, Pennsylvania" Quadrangle at coordinates N 40° 54.7' W 75° 10.4'. A regional location plan of Minsi Lake Dam and reservoir is enclosed as Plate 1, Appendix E.
- c. <u>Size Classification</u>. The dam is classified as an "Intermediate" size dam by virtue of its 1,793 acre-foot total storage capacity.
- d. <u>Hazard Classification</u>. A "High" hazard classification is assigned consistent with the potential for extensive property damage and loss of life downstream, particularly along Martins Creek near Rosetta, Pennsylvania, along PA Route 191.
- e. Ownership. The dam is owned and maintained by the Pennsylvania Fish Commission. All correspondence should be sent to Mr. E. J. Grindall, Senior Project Engineer, Pennsylvania Fish Commission, Division of Engineering, Robinson Lane, Belfont, Pennsylvania 16823.
- f. Purpose of Dam. The reservoir is used as a fishing lake.
- g. <u>Design and Construction History</u>. Test borings for this project were performed by Borings, Soils & Testing Company and F. T. Kitlinsky & Associates, both of Harrisburg,

Pennsylvania. The topographic survey and preliminary design drawings were prepared by Jordan, McNee, Parnum & Yule of Camp Hill, Pennsylvania, in 1965 and 1966. In October 1966, the Fish Commission cancelled the project, apparently because construction bids exceeded the allotted funds. In March 1969, the project proceeded with "Project 500" funds. The State prepared final construction drawings and construction began on July 8, 1969.

In an October 13, 1969 inspection report by Mr. Fisher, remarks indicate that boils were observed in the foundation area. This condition was discussed with DER, who recommended extending the filter blanket over the boils and continuing drainage through the toe of the dam. According to Mr. Roy R. Frank, "It is my opinion that the boils are caused by the high water table in that area and by concentrated impact loads, such as the large earth-moving equipment passing over the area causing it to rise and showing up as boils which seem to dry up when no movement is near. However, I plan to relieve the pressure so that it will not occur later on as a safety factor."

A November 1969 State inspection report notes that density reports on the embankment material were no satisfactory. The resident engineer indicated the tests were improperly performed and material was not compacted with a high moisture content. Also, the contractor was going to use another compactor and better results were expected. Operations were terminated for the winter, resuming again in 1970. Final inspection of the dam was performed on November 6, 1970, and the official inspection date is recorded as November 12, 1970. Contractor for this work was J. H. Beers, Inc. Participating Pennsylvania Fish Commission personnel include Mr. Edward R. Miller, chief engineer; Mr. Roy R. Frank, in charge of design; and Mr. Luke G. Fisher, resident engineer.

h. Normal Operating Procedures. Under normal conditions, reservoir outflow is controlled by a stoplog weir system located in the intake riser. Stoplogs are inserted in tracks inside the tower and the number of stoplogs determines the reservoir level. At the time of inspection, all stoplogs were in place and the elevation of the reservoir was at the level of the emergency spillway crest. Flows exceeding the capacity of the stoplog weirs are discharged over the emergency spillway located at the left abutment of the structure. Since wooden stoplogs are not completely sealed at the joints, water seeps through these joints. The base of the tower also contains a pipe valve, as shown on Plate 7, which is used as a downstream minimum flow release.

1.3 Pertinent Data.

A summary of pertinent data for Minsi Lake Dam is presented as follows.

a.	Drainage Area (sq miles)	3.7
b.	Discharge at Dam Site (cfs) Maximum Known Flood at Site At Top of Dam	Unknown 3,974
c.	Elevation (feet above MSL) Top of Dam Emergency Spillway Crest Intake Tower or Control Tower Stoplog Weir Crest Tower Inlet Invert Outlet Invert Top of Tower	703.5 698.0 698.0 (variable) 677.5 677.0 706.67
d.	Reservoir (miles) Length at Normal Pool Fetch at Normal Pool	0.5 0.5
e.	Storage (acre-feet) Normal Pool/Emergency Spillway Crest To Top of Dam	960 1,793
f.	Reservoir Surface (acres) Normal Pool	117
g.	Dam Data Type Volume Length Maximum Height Top Width Freeboard at Normal Pool Side Slope	Zoned rolled earth Unknown 3,300 feet 26.5 feet 16 feet 5.5 feet
	Upstream Downstream Cutoff Grout Curtain	3H:1V 2.5H:1V 12 foot wide cutoff trench at base under centerline. None
h.	Principal Spillway Type	Standard Fish Com- mission control tow-

er w/ stoplogs.

Minimum Flow

Emergency Drawdown

Elevations
Weir
Inlet Invert
Outlet Invert
Emergency Spillway
Type

Size Side Slopes 2" cast iron pipe & valve for minimum flow release.
2' x 2' orifice at base of tower.

698.0 677.5 677.0

Concrete trapezoidal weir, discharge chute & stilling basin. 80 feet wide Vertical concrete retaining walls.

SECTION 2 ENGINEERING DATA

2.1 Design.

- a. <u>Data Available</u>. A summary of engineering data for Minsi Lake Dam is presented on the checklist attached herein as Appendix A. Principal documents used for this report include inspection reports prepared by representatives of the Pennsylvania Fish Commission, boring logs, foundation report, the "Report Upon the Application of the Pennsylvania Fish Commission" dated April 23, 1969, as well as letters and other miscellaneous correspondence pertinent to the design and construction of the dam. In addition to these documents, there were also 21 photographs in the file covering various phases of construction.
- b. <u>Design Features</u>. Principal design features of the embankment and appurtenant structures are illustrated on the plan, profile and cross-section plates enclosed in Appendix E as Plates 2 through 10. A description of the features is also presented in Section 1.2, "Description of Project".

2.2 Construction.

Based on documentation in DER files and discussions with Pennsylvania Fish Commission representatives, it is believed that the dam was constructed in general accordance with criteria established by the Pennsylvania Fish Commission. It is noted in Section 1.2, paragraph g, that some compaction problems were encountered. These problems were reportedly overcome and satisfactory materials placed in accordance with specification requirements. Construction photographs verified a few details which could not be observed during the field inspection.

2.3 Operational Data.

Minimum flow required by DER is maintained by a valve at the base of the intake tower. The dam and appurtenant facilities were designed to be operated without a dam tender, and no operational data is available. It is understood that the sluice gate is operated yearly with periodic maintenance of the sluice gate hoist.

2.4 Evaluation.

- a. <u>Availability</u>. All engineering data reproduced in this report and studied for this investigation were provided by DER and the Fish Commission.
- b. Adequacy. The data provided was adequate to evaluate the structure in accordance with Phase I inspection criteria.
- c. $\underline{\text{Validity}}$. There is no reason to question the validity of available data.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

- a. General. Observations and comments of the field inspection team are contained in the checklist enclosed herein as Appendix B, and are summarized and evaluated in the following subsections. In general, the appearance of the facilities indicates that the dam and its appurtenances are reasonably well maintained and in good condition.
- Visual inspection revealed no surface cracks b. Dam. other than minor cracking of the asphalt roadway on the crest. There were no unusual movements or cracking at or beyond the toe, neither was there sloughing or erosion of the embankment or abutment slopes. Embankment settlement on the order of five inches was observed around the intake riser, as shown on Photographs 1 and 10, Appendix D. Vertical and horizontal alignments were checked with a transit and found to be excellent. The upstream slope is paved with hand-placed block and is found to be in good condition, except at normal pool elevation where there are signs of deterioration associated with ice and wave action. This condition is shown on Photograph 12, Appendix D. The junction between the embankment and abutment is considered in good condition and there was no seepage observed beyond the downstream toe. conditions with standing water just beyond the downstream toe were observed; but most, if not all, can be attributed to poor drainage and natural topography. There was no evidence observed of seepage through the dam directly. Clear water was discharging from the toe drain outlets.

c. Appurtenant Structures.

- 1. <u>Intake Tower</u>. Exposed portions of the intake tower and outlet structure were inspected and found to be in good condition with no significant spalling, cracking or concrete deterioration. The outlet channel was inspected and found to be in good condition.
- 2. Emergency Spillway. The emergency spillway was observed to be in good condition with no signs of cracking, spalling or concrete deterioration. There was one small shallow surface slide noted on the left cut slope just downstream of the emergency spillway, but this has wo effect on the ability of the spillway to pass flows.

- d. Reservoir. Reconnaissance of the reservoir disclosed no evidence of significant siltation, slope instability or other features that would significantly affect the flood storage capacity of the reservoir. All slopes are well vegetated with grass or trees to the water's edge.
- e. <u>Downstream Channel</u>. The channel downstream of the stilling basin is wide and protected with riprap and assessed to be in good condition. Downstream conditions are further described in Section 5.

3.2 Evaluation.

In summary, visual inspection of the structure disclosed no evidence of apparent past or present movement of the dam or its appurtenant facilities. Seepage or wet areas noted along the downstream toe, as shown on sheet 5a, were traced and assessed to be from natural drainage toward the toe of the dam, possibly from natural springs which are common to this swampy area.

Exposed portions of the intake riser were inspected and observed to be in good condition. The emergency spillway was also assessed to be in good condition.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures.

Normal operating procedures do not require a dam tender. Water level is maintained by a stoplog weir system inside the tower and by the emergency spillway. In the event it is necessary to lower the reservoir, the sluice gate at the base of the control tower can be opened by a hoist at the top of the tower or the stoplogs can be removed.

4.2 Maintenance of the Dam.

The dam is maintained by Pennsylvania Fish Commission personnel. Maintenance normally consists of cutting the grass and replacing concrete block on the upstream slope. As necessary, trash and other floating debris are removed from the shoreline.

4.3 Maintenance of Operating Facilities.

Maintenance of the operating facilities, which include the intake tower and spillway, is also performed by the Pennsylvania Fish Commission. There is evidence to indicate that the control tower is inspected periodically as the hoist was painted, greased and appeared to be functioning properly. Similarly, the spillway was also observed to be in good condition.

4.4 Warning Systems In Effect.

There are no warning systems in effect or procedures specifically established for this structure which are to be followed during exceedingly heavy rainfalls. However, a procedure is being prepared and will be instituted soon.

4.5 Evaluation.

Written operation/maintenance procedures and a warning system are currently being formulated. These draft procedures have been reviewed and appear to be comprehensive, covering the major components of the dam.

SECTION 5 HYDROLOGY/HYDRAULICS

5.1 Evaluation of Features.

a. <u>Design Data</u>. Two sets of hydraulic calculations, both marked "preliminary" were supplied by the Fish Commission. It is apparent from the calculations and DER files that the spillway was designed to discharge the value required by the Department of Forests and Waters' "C" curve. The required discharge of 3,974 cfs was provided. Other calculations made for this investigation are presented in Appendix C.

The small, mountaintop watershed has an approximate length of 2.5 miles and average width of 1.3 miles for a total area of 3.63 square miles. Elevations range from 1,534 feet in the upper reaches (the Appalachian Trail) to 698 at normal pool elevations. The watershed is 80 to 90 percent wooded with a few scattered homes. Runoff characteristics are not expected to change significantly in the near future.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam and "High" hazard classification is the Probable Maximum Flood (PMF).

- b. Experience Data. No reservoir water level records or precipitation records are maintained. There is no estimate of previous high water levels.
- c. <u>Visual Observations</u>. On the date of inspection, there were no conditions observed that would indicate a reduced spillway capacity during a flood occurrence. Other observations regarding the condition of the downstream channel, spillway and reservoir are located in Appendix B and discussed in Section 3.
- d. Overtopping Potential. Overtopping potential of this dam was estimated using "HEC-1, Dam Safety Version", computer program. A brief description of the program and a summary of the dam safety analysis are included in Appendix C. Calculations for this investigation essentially confirm the design spillway capacity, with an estimated discharge of 3,942 cfs, with the reservoir level at the top of the dam. The HEC-1 program computed the peak PMF inflow to be 7,393 cfs. The spillway can pass approximately 70 percent of the PMF without overtopping the embankment.

- e. Spillway Adequacy. The spillway is considered to be "Inadequate" but not "Seriously Inadequate" as the dam will pass more than 50 percent of the PMF without overtopping the embankment.
- f. Downstream Conditions. About 1,000 feet below the outlet of the spillway channel, East Branch Martins Creek passes under LR 48032 and the stream valley becomes wide, flat and marshy. On LR 48032 near the creek are two homes subject to damage in the event of failure. About 5,000 feet farther downstream, the East Branch joins the West Branch and the stream channel becomes narrow and steep. The valley becomes progressively narrower and steeper toward Bangor, about four miles below the dam. Near the intersection of State Route 191 and LR 48089 are several homes subject to damage in the event of dam failure. In conclusion, it is evaluated that significantly greater downstream damage would result from failure of the dam during a PMF than damage resulting from large flows during passage of the PMF.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

a. Visual Observations. Field inspection disclosed no evidence of potential instability of the embankment or its components. Embankment slopes are reasonably uniform with no signs of displacement or sloughing. Settlement of the embankment on the order of five inches was noted adjacent to the control tower. Considering the compaction problems noted and discussed in Section 3, this settlement could be expected.

The condition of the upstream block was assessed to be good, except for isolated places along normal pool level where some deterioration due to frost and waves has occurred. However, this is apparently being cared for on a routine basis. Exposed portions of the intake tower were inspected and judged to be in good condition. Similarly, the emergency spillway was also judged to be in good condition.

There was no exterior evidence indicating abnormal seepage through the embankment. Wet zones at the downstream toe were traced to topographic conditions where surface runoff drains towards the toe of the dam.

b. <u>Design and Construction Data</u>. All available design documentation, calculations and other data received from the Department of Environmental Resources and the Fish Commission were assessed and reviewed. A listing of this data is included herein as Appendix A and discussed in Section 2.

Design documentation was considered adequate to evaluate the structure. The stability analyses in Fish Commission files indicate a factor of safety for steady state seepage conditions in excess of 2.0. Design data included geologic information and a foundation investigation report. Test borings and soil tests performed by various contractors were also reviewed and assessed to be complete.

- c. Operating Records. There are no operating procedures for this dam. However, procedures are currently being prepared and will be implemented in the near future.
- d. <u>Post-Construction Changes</u>. There are no construction changes reported to have been made to this structure since construction.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1. Normally it can be considered that if a dam in this zone is stable under static conditions, it can be assumed safe for any expected earthquake conditions. Since the stability analysis shows a factor of safety for steady state seepage conditions of at least 2.0, seismic stability of the dam has also been satisfied.

SECTION 7 ASSESSMENT/REMEDIAL MEASURES

7.1 Dam Assessment.

- a. <u>Evaluation</u>. Visual inspection and review of design and construction documentation indicate the dam, foundation and appurtenant facilities of Minsi Lake Dam are in reasonably good condition. The hydrologic/hydraulic computations presented in Section 5 and Appendix C indicate the dam will pass about 70 percent of the Probable Maximum Flood without overtopping. Therefore, the spillway system for this structure is considered to be "Inadequate". In the event of failure, significantly more property damage would be expected than just prior to failure as a result of high flows. Since the structure is located upstream of several populated areas, it is considered a "High" hazard potential dam.
- b. Adequacy of Information. Combined design information, construction data, visual inspection and obvious performance history of this structure were sufficient to evaluate the dam and appurtenant facilities.
- c. Need for Additional Studies. At the present time, it is not believed that additional studies are necessary.
- d. <u>Urgency</u>. It is concluded that recommendations presented in Section 7.2 be implemented as soon as practical.

7.2 Remedial Measures.

- a. <u>Facilities</u>. The following recommendations are presented. All engineering evaluations for corrective work or the need for corrective work should be reviewed by a registered professional engineer experienced in the design of dams.
 - 1. The marshy area at the toe of the structure should be regraded and drained away from the dam. Subsequently, seepage should be monitored to determine whether it flows through the embankment. Should it be determined that seepage flows through the embankment, appropriate remedial measures should be taken to control this flow.
 - Concrete block on the upstream slopes should continue to be monitored, especially during the spring of each year. Deteriorated block should be removed and replaced with new block.

b. Operation and Maintenance Procedures. Operation/maintenance and warning procedures, which have been written by the Fish Commission, should be established as soon as practical. They should include procedures for monitoring the structure during the passage of unusually large flows and should include provisions for warning or evacuating downstream residents, if conditions warrant.

APPENDIX

1

A

CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPENATION PHASE I

Minei Dam NAME OF DAM

PA 00788 # QI

ITEM

AS-BUILT DRAWINGS

REMARKS

Sheet 1 of 4

1968 design drawings are available as found in DER files.

REGIONAL VICINITY MAP

See Plate 1, Appendix E.

CONSTRUCTION HISTORY

See Section 1.2 paragraph "g" of report.

TYPICAL SECTIONS OF DAM

See Appendix E.

OUTLETS - PLAW

DETAILS

CONSTRAINTS

DISCHARGE RATINGS

RAINFALL/RESERVOIR RECORDS

See Appendix E.

- See Section 5 and Appendix C.

- Not available.

	P 10 7 1990C
ITEM	KEMAKAS
DESIGN REPORTS	1. Foundation report submitted to DER (11 Feb. 66) by consultant but the document could not be located in DER files. 2. Document was reviewed in Fish Commission files.
GEOLOGY REPORTS	1. Geology data is presented in the "Report Upon the Application", 23 April 1969. 2. Additional geologic data is presented in Appendix F. 3. Design Geologic data found in Foundation Report located in Fish Commission files.
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY (1) SEEPAGE STUDIES	- Not available in DER files Stage-storage cases in DER files. Not available in DER files. Not available in DER files. Dam Stability: End of Construction - F.S. = 2.76 Steady State F.S. = 2.00 Steady State F.S. = 2.00
MATERIALS INVESTIGATIONS BORING RECORDS	Test Borings by "Boring Soils and Testing Company" and F.T. Kitlinski and Associates in DER files.
POST-CONSTRUCTION SURVEYS OF DAM	None.
BORROW SOURCES	- Soil tests by F.T. Kitlinski and Associates.

MARKS Sneet 3 or

MONITORING SYSTEMS

MODIFICATIONS	None.
HIGH POOL RECORDS	unknown.
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None.

PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS

None.

Yes. Data reviewed in Fish Commission files. Operational, Maintenance Manual and Warming Procedures were also found and reviewed in Fish Commission files.

MAINTENANCE OPERATION RECORDS

	Sheet 4 of 4
ITEM	REMARKS
SPILLWAY PLAW SECTIONS DETAILS	See Appendix E.
OPERATING EQUIPMENT PLANS & DETAILS	See Appendix E.
MISCELLANEOUS	1. "Application of the Commonwealth of Pennsylvania", 12 March 1969. 2. "Report Upon the Application of the Pennsylvania Fish Commission", April 23, 1969. 3. Pennsylvania Fish Commission Resident Engineer reports by Mr. Roy R. 4. Inspection Reports by DER with 21 black and white photographs.

. Frank.

APPENDIX

В



0

CHECK LIST VISUAL INSPECTION PHASE I

Sheet 1 of 11

State Pennsylvania ID # PA 00788 I-High	ature 40's	Tailwater at Time of Inspection N/A M.S.L.	John H. Frederick (Geotechnical)	Recorder	ennsylvania Fish Commission were
County Northampton Sta	April 1979Weather Clear, cool, Temperature windy	698 M.S.L.	al) Mary F. Beck (Hydologist) Vincent McKeever (Hydraulic)	John Boschuk, Ir.	Messrs. E.J. Grindall and R. Stickler from the Pennsylvania Fish Commission were present and provided assistance.
Name Dam Minsi Dam Type of Dam Rolled earth	Date(s) Inspection 19 April 1979	Pool Elevation at Time of Inspection	Inspection Personnel: John Boschuk, Jr. (Geotechnical) Raymond Lambert (Geologist)		Remarks: Messrs. E.J. (present and pi

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF ANY NOTICEABLE SEEPAGE	OBSERVATIONS N/A	Sheet 2 of 11 REMARKS OR RECOMMENDATIONS
STRUCTURE TO ABUTAENT/EMBANKMENT JUNCTIONS	N/A	
DRAINS	N/A	
WATER PASSAGES	N/A	
FOURDATION	N/A	

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF	0BSERVATIONS	Sheet 3 of 11 REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	N/A	
STRUCTURAL CRACKING	N/A	
VERTICAL AND HORIZONTAL ALIGNMENT	N/A	
MONOLITH JOINTS	N/A	
CONSTRUCTION JOINTS	N/A	

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 4 of 11 REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed. Minor cracking of the asphalt walkway on the crest was noted but this does not effect the structure.	walkway ct the
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None observed.	
SLOUGHING OR EROSION OF EMBANDIENT AND ABUTHENT SLOPES	None observed.	
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	Excellent.	
RIPRAP FAILURES	None observed. Upstream slope is protected with concrete block. At normal pool level this block shows signs of deterioration from ice and wave action. See photograph in Appendix D.	ted with concrete shows signs of See photograph in

EMBANKMENT

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS	JUNCTION OF EMBANKMENT Good condition. AND ABUTMENT, SPILLWAY AND DAM
VISUA	JUNCT AND AND A

None. STAFF GAGE AND RECORDER

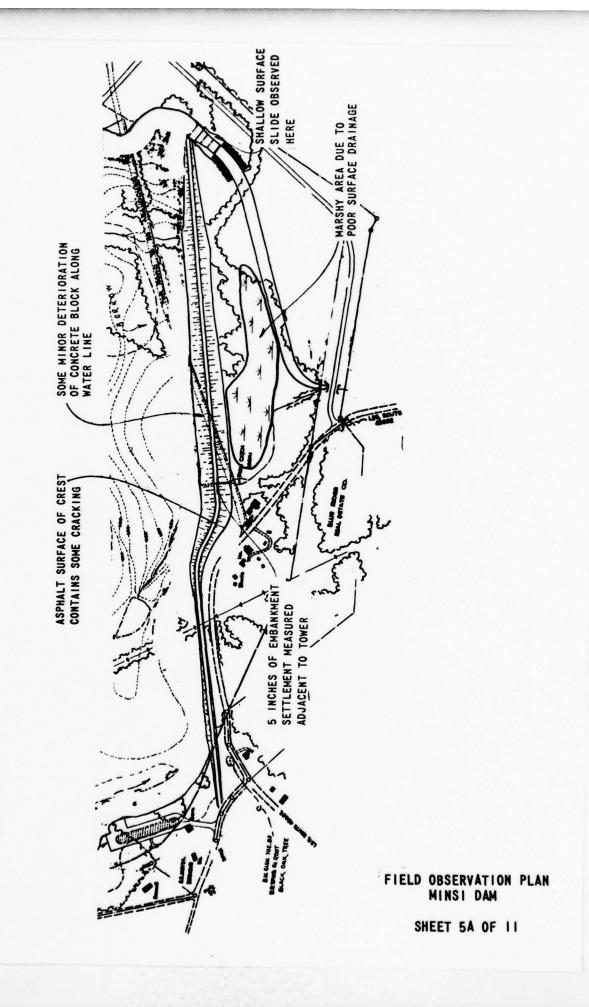
None observed. The marshy areas with standing water just beyond the downstream is attributed to poor drainage and the natural topography. There was no evidence found of seepage through the

topography. dam.

ANY NOTICEABLE SEEPAGE

Clear toe drain discharge through the principal spillway outlet structure and was observed and assessed to be functioning as designed.

DRAINS



OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 6 of 11 REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	None observed.	
IMTAKE STRUCTURE	The accessable portions of the riser were inspected and observed to be in good condition. Settlement on the order of 5 inches was noted around the intake structure as shown on the photographs in Appendix D.	vere inspected and observed on the order of 5 inches as shown on the photographs
OUTLET STRUCTURE	Good condition.	
OUTLET CHANNEL	Good condition.	
EMERGENCY GATE	Good condition.	

UNGATED SPILLWAY

		Sheet 7 of 11
VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OF	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	Good condition.	
APPROACH CHANNEL	Good condition.	
DISCHARGE CHAINEL	Good condition.	
BRIDGE AND PIERS	N/A	

GATED SPILLWAY

		Sheet 8 of 11
VISUAL EXAMINATION OF CONCRETE SILL	OBSERVATIONS N/A	REMARKS OR RECOMMENDATIONS
APPROACH CHAMNEL	N/A	
DISCHARGE CHANNEL	N/A	
BRIDGE AND PIERS	N/A	
GATES AND OPERATION EQUIPMENT	N/A	

INSTRUMENTATION

		Sheet 9 of 11
VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
P I E Z OMETERS	None	
отнея	None	

RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OR RECOMMENDATIONS
SLOPES	Reservoir side slopes flat, well vegetated with trees and

SEDIMENTATION

Minimal, no effect on flood storage.

DOWNSTREAM CHANNEL

		Sheet 11 of 11
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	The channel downstream of the stilling basin is wide, protected by riprap and in good condition.	is wide, protected by

SLOPES The valley gradient is approximately 0.0025.		
y gradient is app	0.0025.	
y grad	approximately	
y grad	1.8	
SLOPES The valley	gradient	
SLOPES The	valley	,
SLOPES	The	
SLOPES		

APPROXIMATE NO. OF HOMES AND POPULATION

About 1500 feet below the dam are two houses built in flood plain. About 3.5 miles below the dam are several more houses. The stream then enters Bangor, Pennsylvania.

APPENDIX

C

MINSI DAM CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: Mountain top, 80% wooded, less than 5%
residential development. ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 698.0 feet (960 Acre-Feet).
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 703.5 feet (1793 Acre-Feet)
ELEVATION MAXIMUM DESIGN POOL:
ELEVATION TOP DAM: 703.5 feet.
SPILLWAY
a. Elevation698.0 feet.
b. Type Trapazoidal weir.
c. Width80 feet.
d. Length About 150 feet.
e. Location Spillover <u>Left abutment</u>
f. Number and Type of Gates
OUTLET WORKS:
a. Type Standard Fish Commission intake tower.
b. Location Station 17 + 65.
c. Entrance inverts 697.5 feet.
d. Exit inverts 677.0 feet
e. Emergency draindown facilities A 24" by 24" sluice gate at the bottom
of the tower. HYDROMETEOROLOGICAL GAGES:
a. Type None.
b. Location
c. Records
MAXIMUM NON-DAMAGING DISCHARGE: Not estimated.

HEC-1, REVISED FLOOD HYDROGRAPH PACKAGE

The original "Flood Hydrograph Package" (HEC-1), developed by the Hydrologic Engineering Center, Corps of Engineers, has been modified for use under the National Dam Inspection Program. The "Flood Hydrograph Package (HEC-1), Dam Safety Version", hereinafter referred to as, HEC-1, Rev., has been modified to require less detailed input and to include a dam breach analysis. The required input is obtained from the field inspection of a dam, any available design/evaluation data, relatively simple hydraulic calculations, or information from the USGS Quandrangle maps. The input format is flexible in order to reflect any unique characteristics of an individual dam.

HEC-1, Rev. computes a reservoir inflow hydrograph based on individual watershed characteristics such as: area, percentage of impervious surface area, watershed shape, and hydrograph characteristics determined from regional correlation studies by the Corps of Engineers, Baltimore District. The inflow is routed through the reservoir using spillway discharge data obtained from the field inspection or design data. Flood storage capacity is determined from USGS maps or design information and verified by the field inspection. In the event a spillway cannot discharge 0.5 PMF without overtopping and failure of the dam, downstream channel characteristics obtained from the field inspection and USGS maps are inputed and flows are routed downstream to the damage center and a dam breach analysis is performed.

Included in this Appendix are the HEC-1, Rev. pertinent input values and a summary print-out tables.

	DATE 5/23/79	. SUBJECT	SHEET <u>3</u> OF <u>8</u>
IKD. BY	DATE	Minis Lake Dam	JOS No
	/	Hydrology Hydraulics	
TITIT	11111		
Class	Candia (Par Paraman And Ruid !	nias la Salati
Class	Tricenor (Ref - Recommended Guideling Inspection of Dams)	nes for Safety
1.	The hazara	potential is "High" as	failure would result
	in 1055 at	life	16-14-2 DOLLO 15-1-1
2.	The size	classification is "Intermed total storage capacity	liate" based on its
	1793 Az-1	+ total storage capacity	
3.	The apillu	ay design flood, based of	on size and hazard.
	classifica	tion, is the Probable Ma	ximum Flood (PMF).
	1 1 1 1 1 1		
++,,,,	1 + + + , ,		
Hydri	plogy and r	ydraulic Analysis	
++++	4:10		1 1 1 1 1 1
1.	Original D	esign Data - The spillway	was designed to dis-
++++	change not	Tess than 3974 cfs, the	re required discharge
++++++	and Water	so mile drainage area a	ha the Dept. of Poresis
		weir is 80 H. long	
		C = 3.82	
		maximum H = 5.5 ft.	
2.	E valuation	conjuter input data a	e of the computer
	program.	Computer input data a	s follows:
	Intlow	Hydrograph	
	rainta	1, shown on sheet 6.	Ket - Hydrometerological
++++	Kep	ge area, determined from US	20 10 4 11 4 22
	Souder	budge and Dang was few	10 500 Samiles - USE 3.7
	to	s hydrograph parameters : Ct (1.16a) 0.3 Information	s, <i>tp</i> ; <i>tp</i>
	1	C1 : 123) Information	in received from Corps of
		Cp . 0.45) Engineers,	Baltimore for Zone 1
		L = 3,125 miles 1 fm	am USES
		La: 1,515 miles & m	
	to	: 1.96	
		r Routing	
	eleva	tion storage, shown on	sheet 7.
	7	ormal storage from "App lood storage measured !	olication Keport
	+++++++	and enclosed as Plate	rom drawing dated 4-10-66
		uno enciased as plate	- HOOFALLE C

	MFB DATE 5/23/25		SHEETOF
KD. 8Y	DATE	Minis Lake Dam	JOB No
	- V	Hydrology / Hydroulics	
TT	·		
+ + -	eleva	hon discharge, calculated	
	by	computer opporan	+ + 1 + + - 1
		computer program. L. Bott field c C. 3.B2 Table 5.	hecked
		C. 3.82 Table 5.	9 Romber & King
		Hand bo	ok of Hydraulics
	Overtop	nina Potential - as shown on	sheet 8, the
	dam	oing Potential - as shown on overtopped by 0.7 PMF.	
	Spillway	with out overtopping the dam, as "Inadequate" but not "	discharges about
	0.68PMF	with out overtopping the dam,	the spillway is
	rated	as "Inadequate" but not "	Seriously Inadequate."
		+++++++++++++++++++++++++++++++++++++++	
-			
+-+-	 		
+-+-			
+			
+			
+			
++-			
		+ + +	
+-+-			
+ + -			
++-			
			
111			
1			
-			

RUN DATE* 79/05/24. TIME* 10.09.26. NINIS LAKE DAM NAT ID NO. PA 00788 DER NO. 48-139 DVERTOPPING ANALYSIS

			JOB SPEC	JOB SPECIFICATION	×.	
~	ZIZZ	IDAY	IHE	ININ	METRC	IPLT
0	5	0	0		0	0
		JOPER	-32	LROPT	TRACE	
		u->	0	0	0	

150

NSTAN

IPRT -4

> MULTI-PLAN ANALYSES TO BE PERFORMED NPLAN= 1 NRTIO= 6 LRTIO= 1 RTIOS= .50 .60 .70 .80 .90 1.00

SUB-AFEA SUNDEF COMPUTATION

I
چ
GR
8
æ
2
=
3
3
ヹ
2
_

						501	226.	102.	46.	21.	6	÷
E IAUTO	LOCAL		RTIME 0.00			VOL= 1.00	245.	110.	50.	22.	10.	ئ
INAME ISTAGE	ISAME LI	R96	ALSMX 0.00					120.	54.	24.	=:	ຕໍ
JPRT INF	NONSI	R72 0.00	TL CMSTL		RTIOR= 2.00	1.97 HOURS, CP= .45		129.	58.	26.	12.	۶.
JPLT 0	RATIO 0.00v	R48	RIIOK STRTL 1.00 1.00	ATA NTA= 0	50						13.	. 9
ITAPE 0	HYDROGRAPH DATA TRSDA TRSPC 3.70 0.00	PRECIP DATA R12 R24 24.00 134.00	LOSS DATA STRKS RT 0.00 1	UNIT HYDROGRAPH DATA	RECESSION DATA ORCSN=	HYDROGRAPH 71 END-OF-PERIOD ORDINATES, LAG=		-	.89		4.	. 9
IECON	HYDROGRA SNAP TRSDA 0.00 3.70	-	LOS ERAIN S 0.00	UNIT HYD		IOD ORDINA					-	
ICOMP	3.70 0.0	PHS R6	RTIOL	TP=	10= -1.50	VD-OF-PER	364	164.	74.	33.	15.	7
ISTAU IN	IUHG TAF	.806	DLTKR 0.00		STRT@=	APH 71 E	394.	178.	80.	36.	16.	7.
	HYDG 1	SPFI 0.00 PROGRAM IS	STRKR 0.00				427.	193.	87.	39.	18.	&
		ID BY THE	LROPT			TINU	462.	209.	94.	42.	. 6.	6
		TRSPC COMPUTED BY THE										
		TRSP										

SUM 24.99 22.62 7.37 195016. (635.)(575.)(60.)(5522.24)

CONP Q

5807

RAIN EXCS

HR.NN PERIOD

END-OF-PERIOD FLOW COMP Q NO.DA

5507

EXCS

RAIN

MO.DA HR.MN PERIOD

HYDROGRAPH ROUTING

OUTFLOW HYDROGRAPH

			ISTAR	TCOMP	IECO)	ITAP	E JPL	1 JP!	RANI TA	JPRT INAME ISTAGE IAUTO	IAUTO	
			190		~) niting n	\$ T \$	0	0	1 0	٥	
		85070	55073	AVG		S ISAM	IRES ISANE IOPT I	T IPHP	ā,	LSTR		
		0.0						0	0	0		
			NSTPS	NSTDL	LAG 0	9 AMSK	AMSKK X TSK 0.000 0.000 0.000	0.00 ×	SK STORA 0 -698.	A ISPRAT		
CAPACITY=	0	٥	.096	1793.	2972.							
ELEVATION=	.089		.869	704.	708.							
		3 9	CREL 5	SPUID 80.0	3.8	EXPU ELEVL	0.0	0.0	CAREA 0.0	EXPL 0.0		
					703.5	000 S	DAM DATA COMD EXPD 5 0.0 0.0	M DATA EXPD DAMUID 0.0 0.0	£.			
CREST LENGTH	27	273.	3027.	3300.		3300.						
ELEVATION	703.5		703.7	703.8	0.90/	0.5						

43.75 43.50 43.50 42.75 42.75

0.00 0.00 1.50 3.00 4.25

2810. 3446. 4084. 5167. 6148.

1625. 1722. 1815. 1871. 1901.

0.00

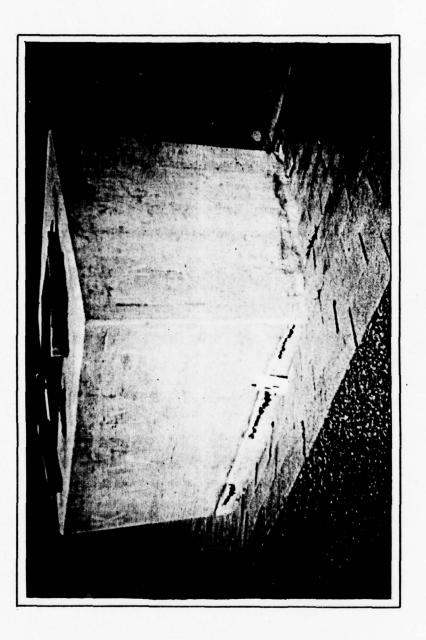
702.39 703.03 703.58 703.80 703.91

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS FLOW AND FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND) AREA IN SQUARE MILES (SQUARE KILOMETERS)

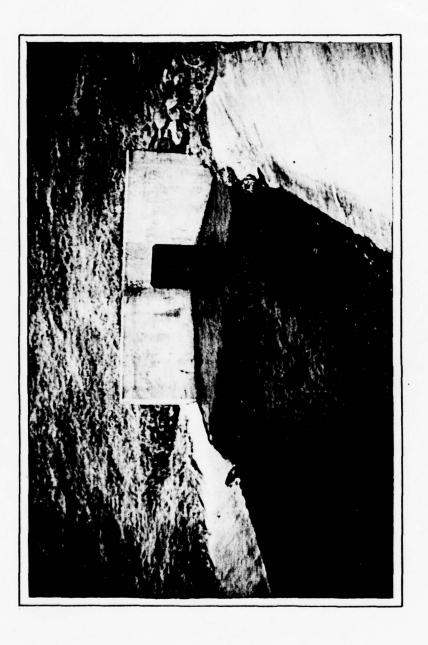
					TIME OF FAILURE HOURS
RATIO 6 1.00	7393.	7039.		£ 0	TIME OF MAX OUTFLOU HOURS
OUS RATIO 5	6654.	6148.		10P OF DAM 703.50 1793. 3942.	DURATION BVER TOP MA) HOURS
ED TO FL TIO 4	5914.	5167.	ANALYSIS	CREST .00 50.	
TIOS APPLI 1110 3 RA .70	5175.	3446. 4084. 5167. 97.57)(115.64)(146.32)(a SAFETY	SFILLWAY CREST 698.00 960.	HAXIMUM OUTFLOW CFS
KATIOS APPLIED TO FLOWS RATIO 1 RATIO 2 RATIO 3 RATIO 4 RATIO 5 RATIO 6 .50 .60 .70 .80 .90 1.00		3446.	SUMMAKY OF DEM SAFETY AWALYSIS	INITIAL VALUE 698.00 960.	MAXIMUM STORAGE AC-FT
8ATIO 1 R	3696. 4436. 104.67)(125.60)(2810.	S	INITIA 69	HAXINUN DEPTH OVER DAM
PLAN	_ ~	- ~		ELEVATION Storage Outflow	MAXIMUM RESERVOIR W.S.ELEV
AREA	3.70	3.70			če
STATION	Z.	TUO ,			RATIO OF PMF
	A			-	
OFERATION	HYDROGRAPH AT	ROUTED TO	-	PLAN	

APPENDIX

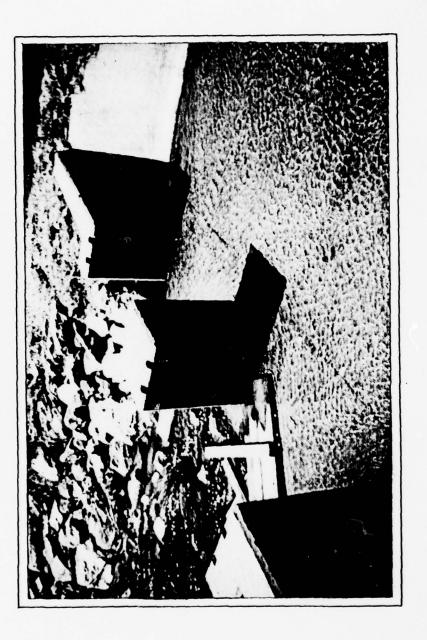
D



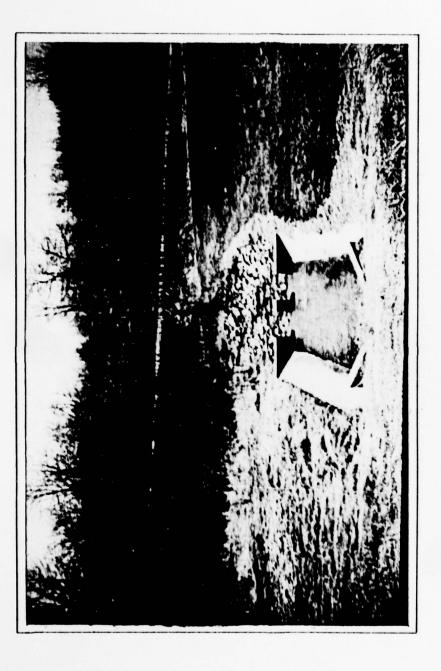
OVERVIEW OF PRINCIPAL SPILLWAY . INLET STRUCTURE.



OVERVIEW OF PRINCIPAL SPILLWAY OUTLET STRUCTURE.



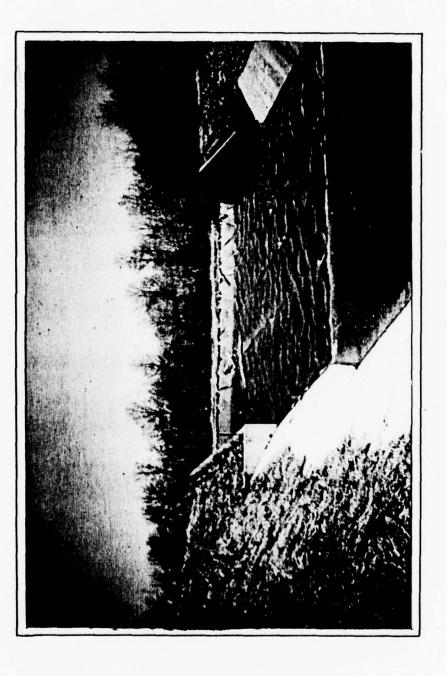
STILLING BASIN OF PRINCIPAL SPILLWAY. NOTE TRACKS IN STRUCTURE FOR FLASHBOARDS FOR INSTALLATION AS FISH CATCH BASIN.



OVERVIEW OF PRINCIPAL SPILLWAY STILLING BASIN AND DISCHARGE CHANNEL.



OVERVIEW OF EMERGENCY SPILLWAY LOOKING TOWARDS THE LEFT ABUTMENT.



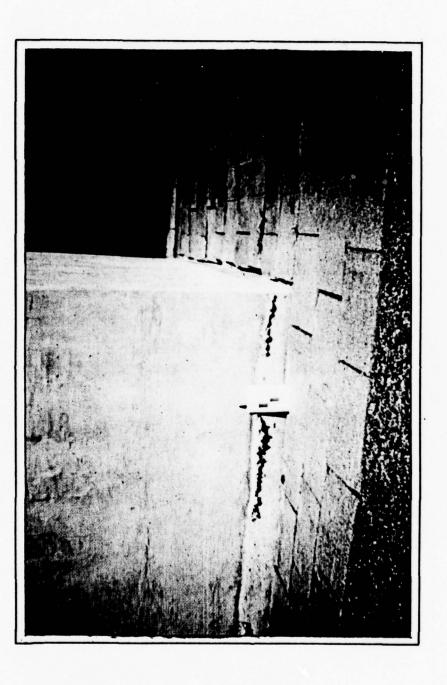
EMERGENCY SPILLWAY LOOKING UPSTREAM.

OVERVIEW OF EMERGENCY SPILLWAY DISCHARGE CHANNEL.

TYPICAL VIEW OF UPSTREAM SLOPE PROTECTED WITH CONCRETE BLOCKS.



TYPICAL VIEW OF DOWNSTREAM SLOPE.



SETTLEMENT AROUND THE PRINCIPAL SPILLWAY INLET TOWER. SETTLEMENT AVERAGED ABOUT FIVE INCHES.



SURFACE SLIDE ON CUT SLOPES, LEFT SIDE OF EMERGENCY SPILLWAY.

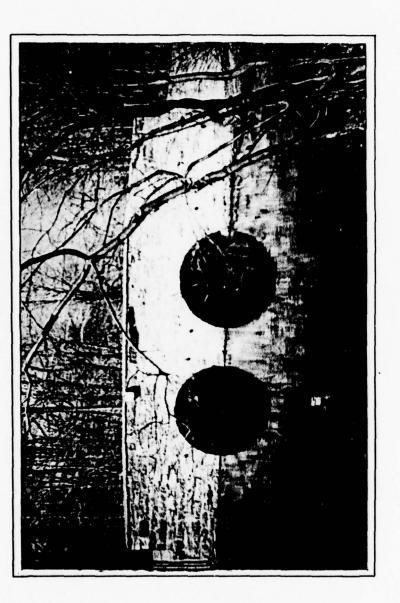


TYPICAL CONDITION OF CONCRETE BLOCK SLOPE FACING AT NORMAL POOL ELEVATION.



DRAINAGE CULVERT ALONG DOWNSTREAM TOE OF DAM ADJACENT TO ROADWAY. THE EMBANKMENT IS ON THE RIGHT AND THE ROAD ON THE LEFT.

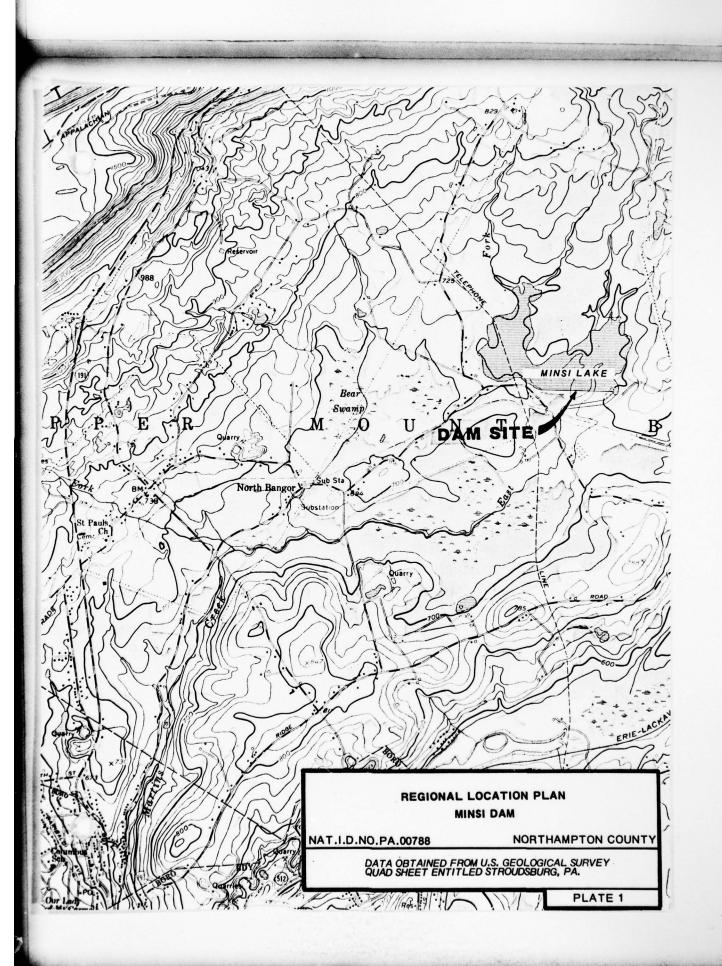
STAGNANT WATER ALONG THE TOE OF DAM CAUSED BY POOR SURFACE DRAINAGE AWAY FROM STRUCTURE.

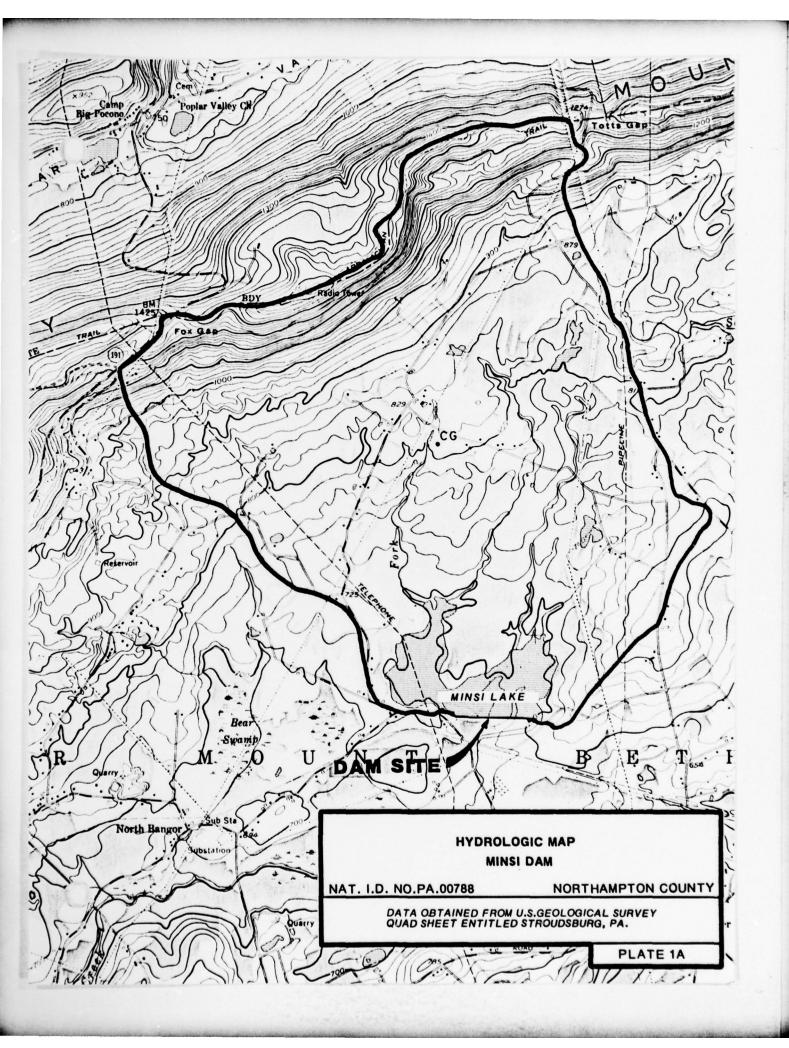


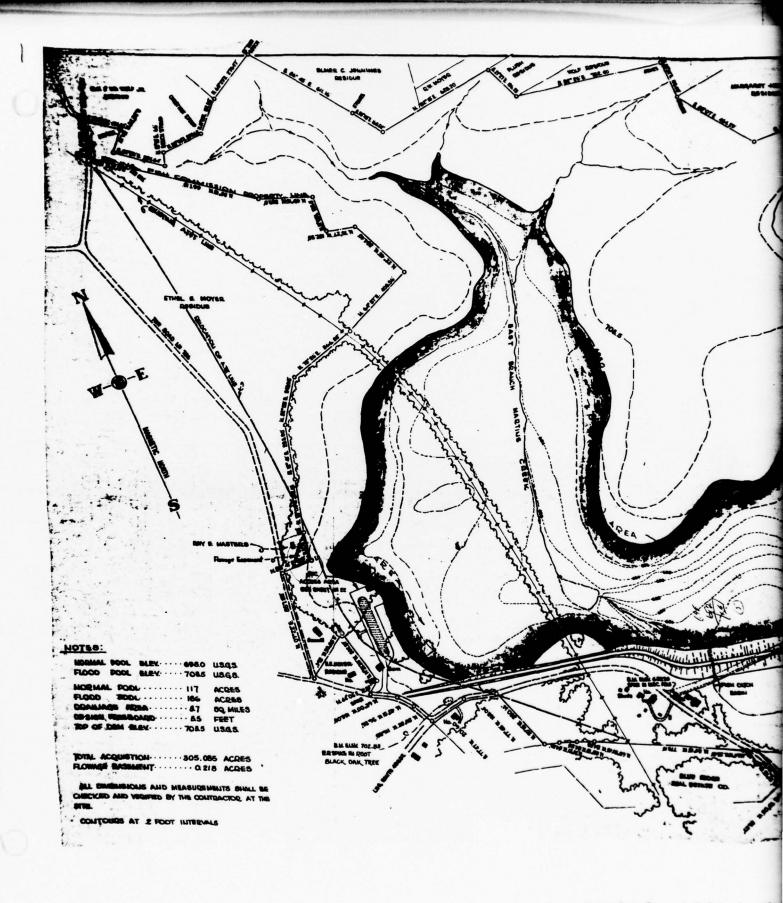
VIEW OF DOWNSTREAM BRIDGE.

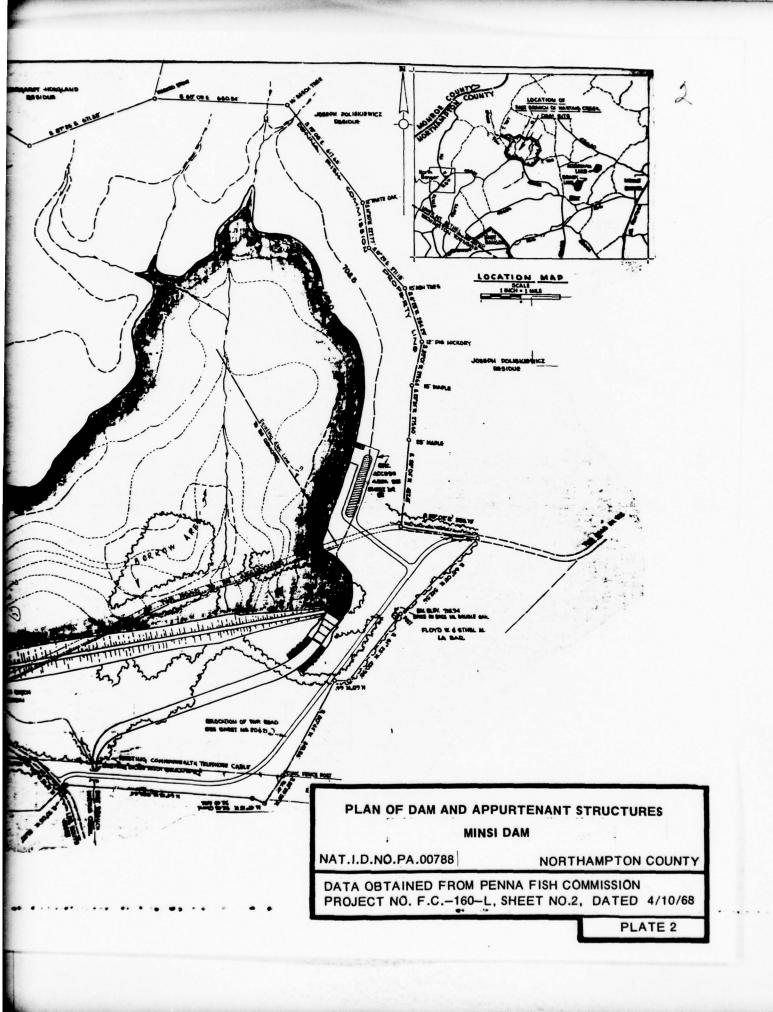
APPENDIX

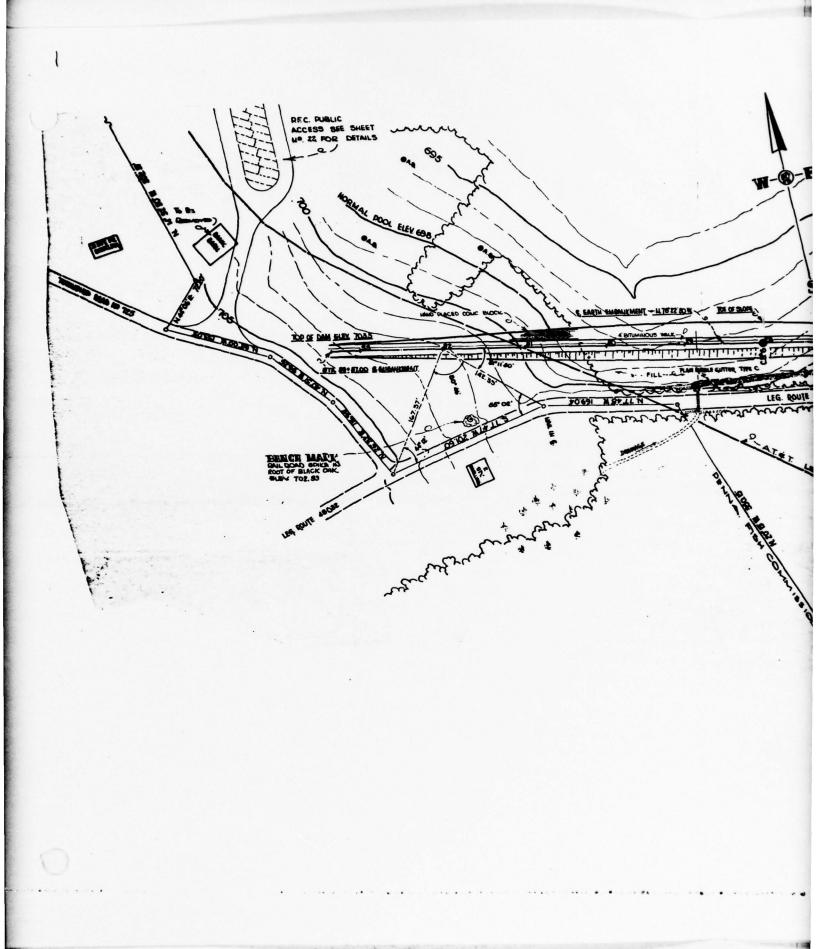
E

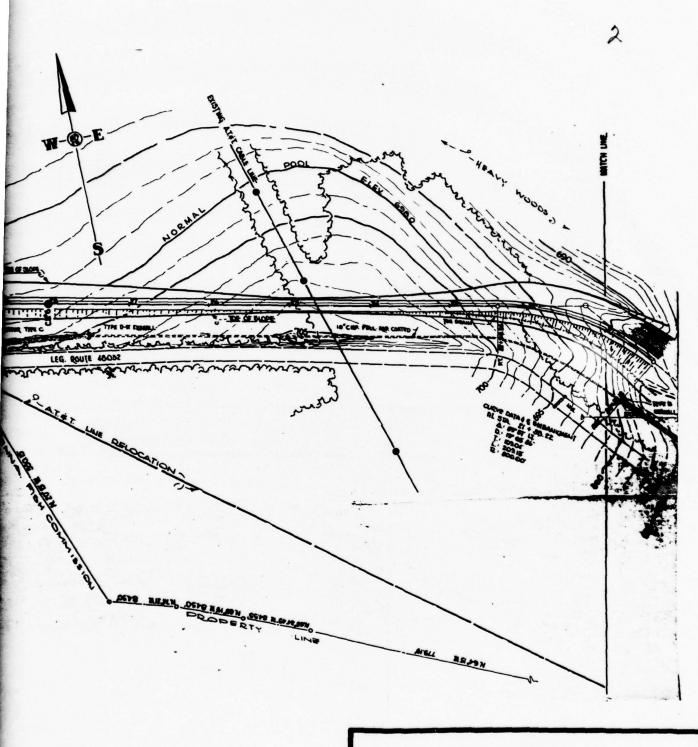












EMBANKMENT PLAN MINSI DAM

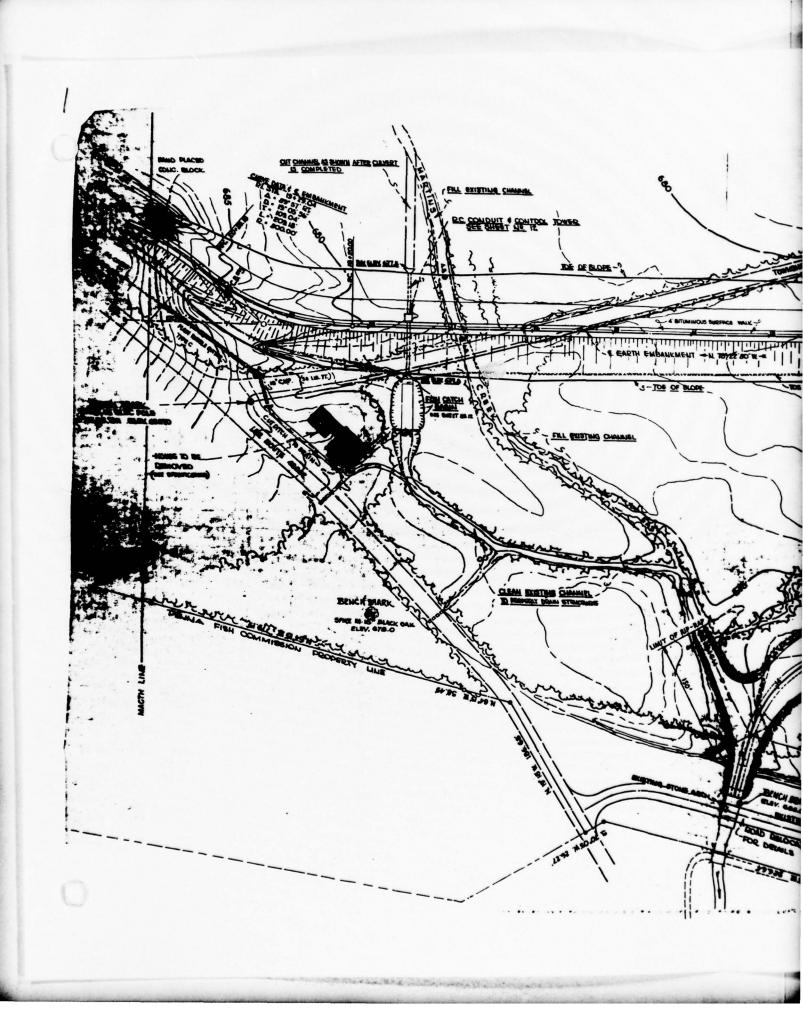
NAT.I.D.NO.PA.00788

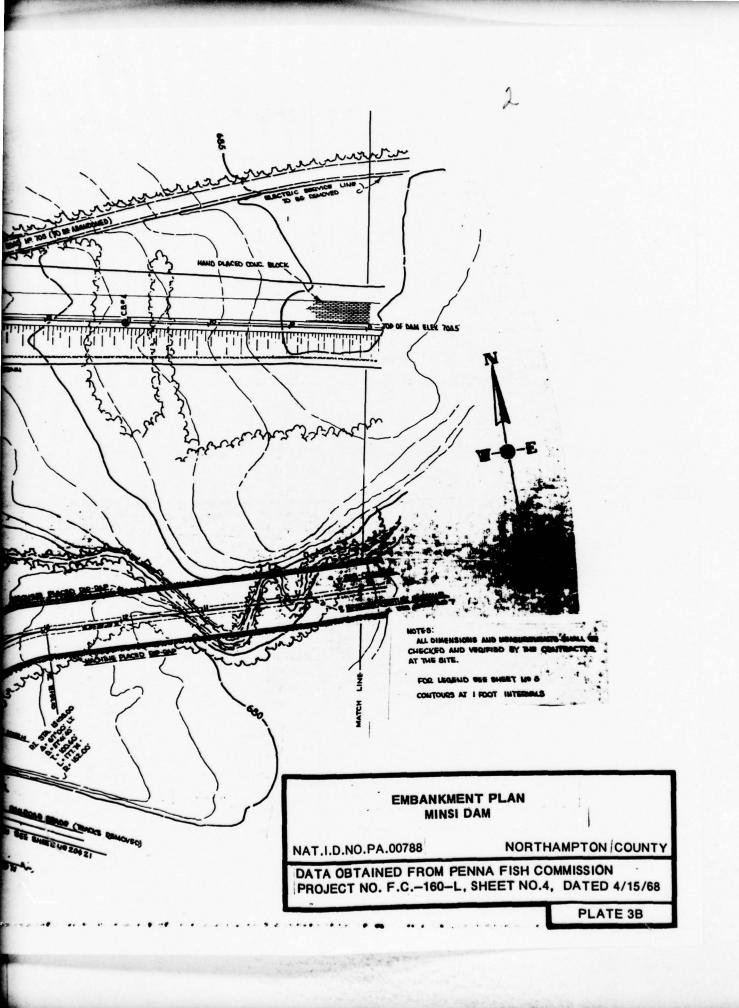
the manufacture of the

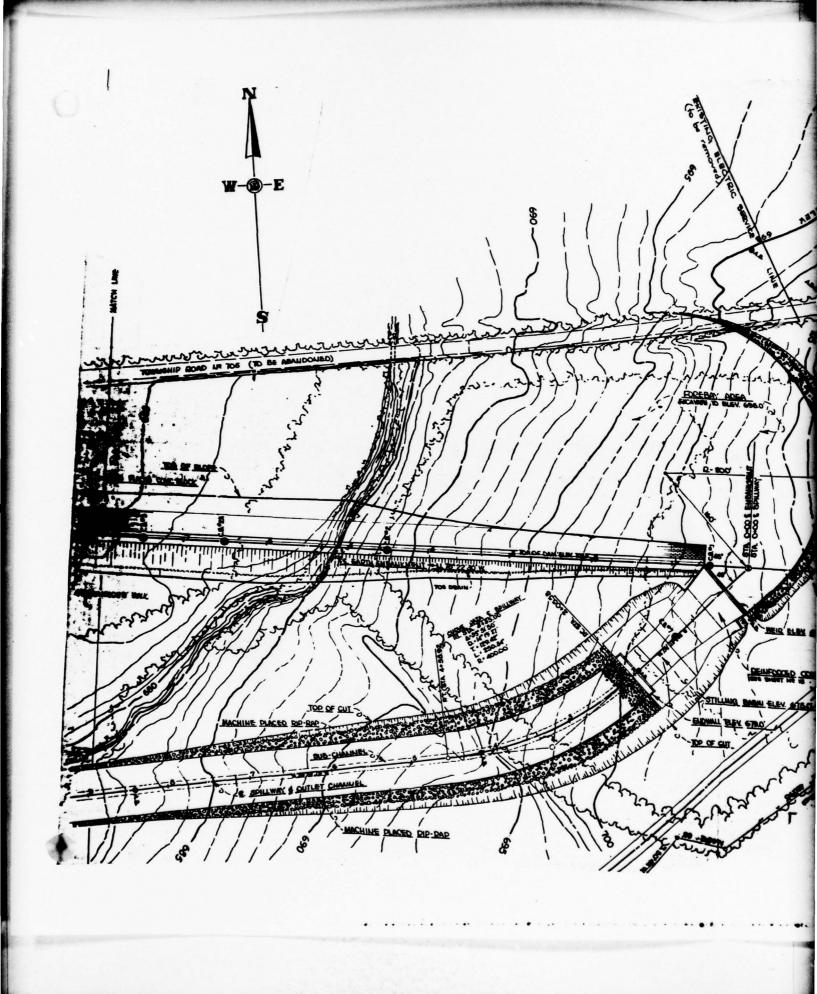
NORTHAMPTON COUNTY

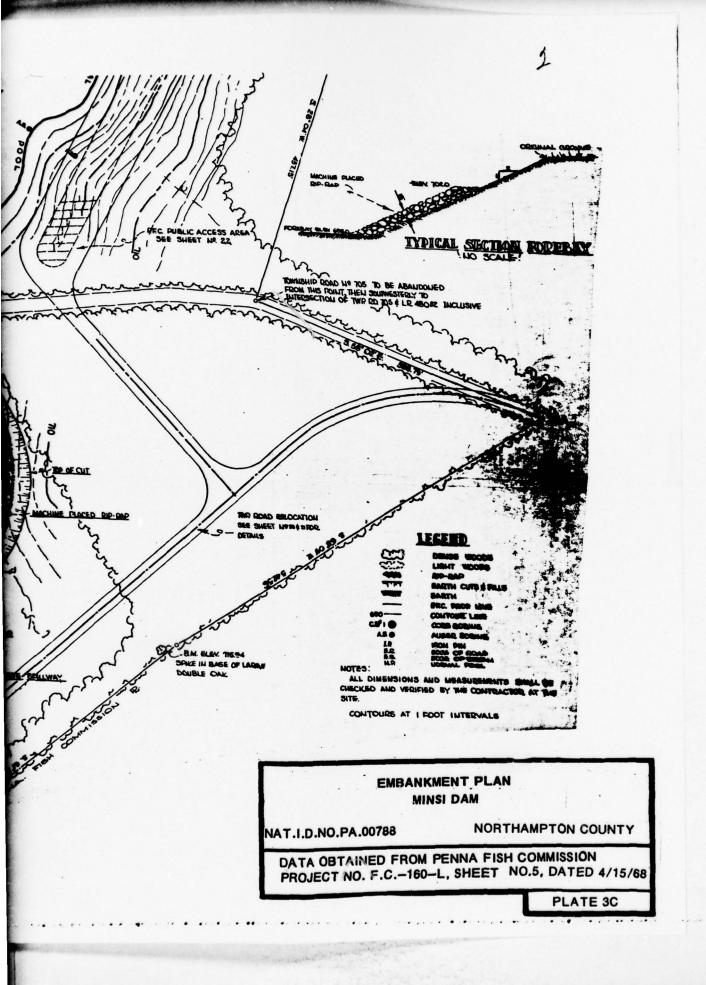
DATA OBTAINED FROM PENNA FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.3, DATED 4/10/68

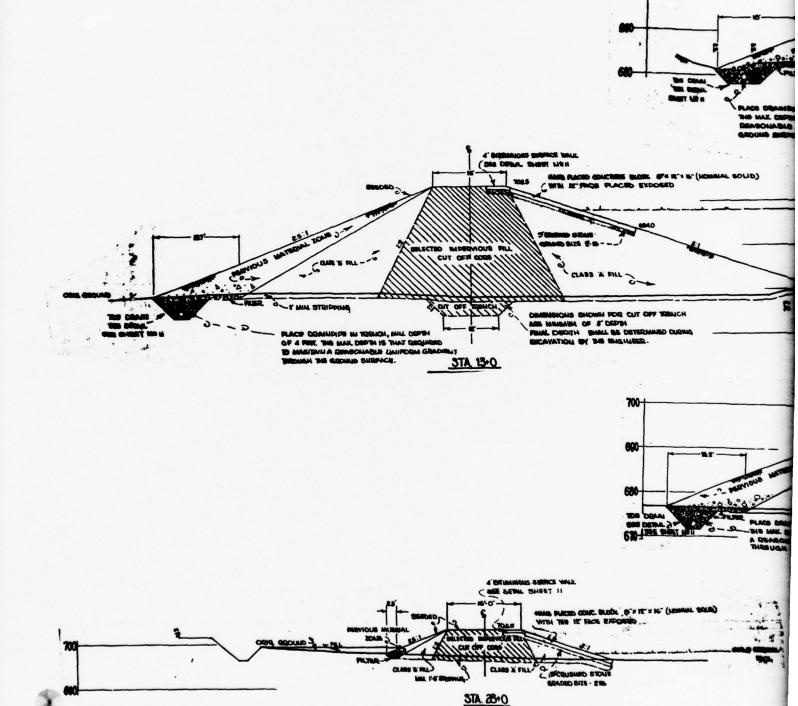
PLATE 3A

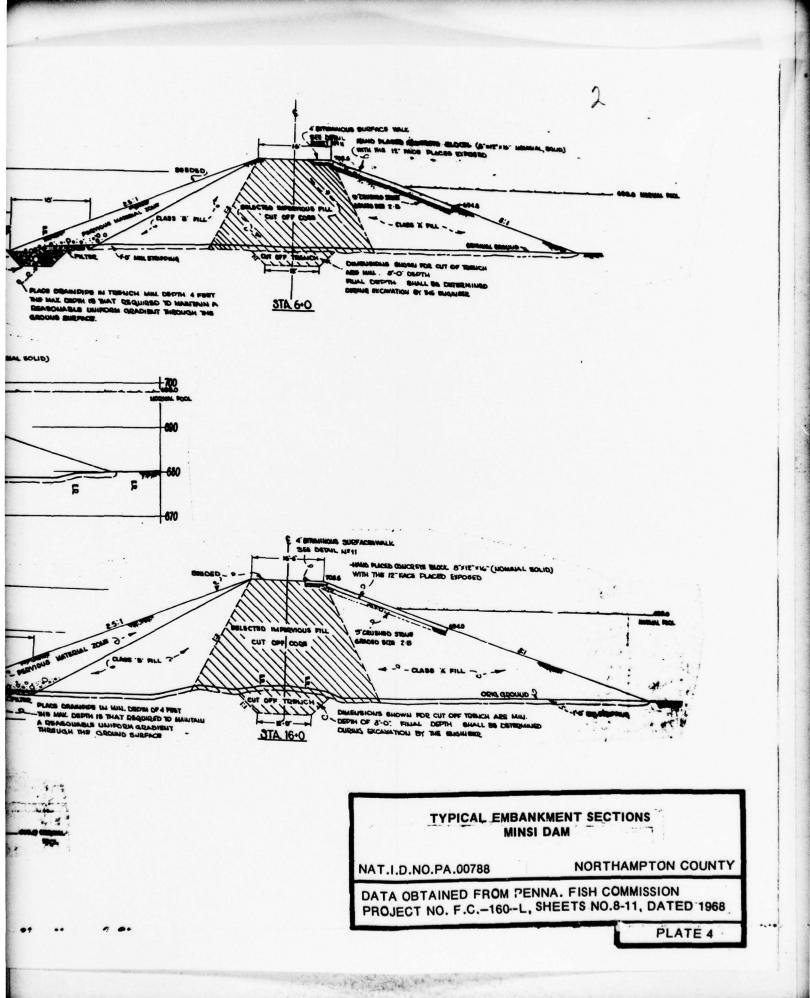




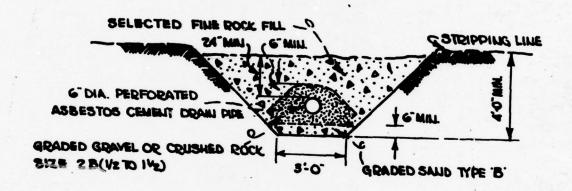








FILTER MATERIAL



DETAIL TOE DRAIN INSTALLATION

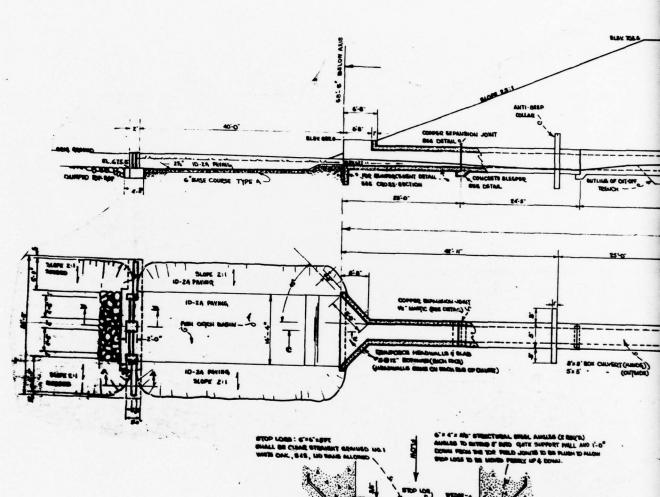
DETAIL TOE DRAIN INSTALLATION
MINSI DAM

NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

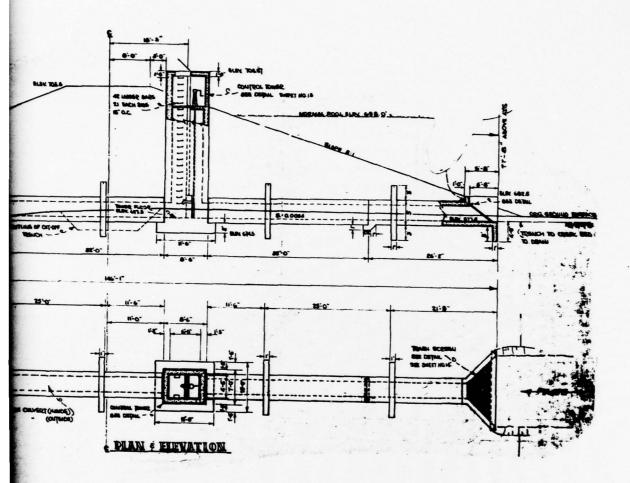
DATA OBTAINED FROM PENNA. FISH COMMISION PROJECT NO. F.C.-160-L, SHEET NO.11, DATED 5/4/68

PLATE 5 .



Designation of the property of

STOP LOG GROOVE

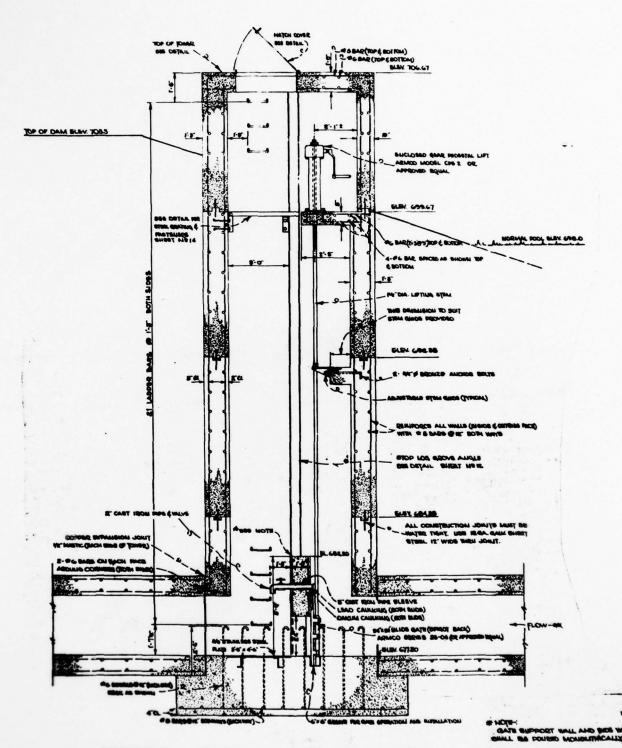


PLAN AND PROFILE OF OUTLET WORKS MINSI DAM

NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

DATA OBTAINED FROM PENNA. FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.12, DATED 4/10/68



DETAILED SECTION & CONTROL TOWER

- 17 AND CO

מספייליר נססל מיציג פטפים

CONTRACTOR PRICES

-

- From-

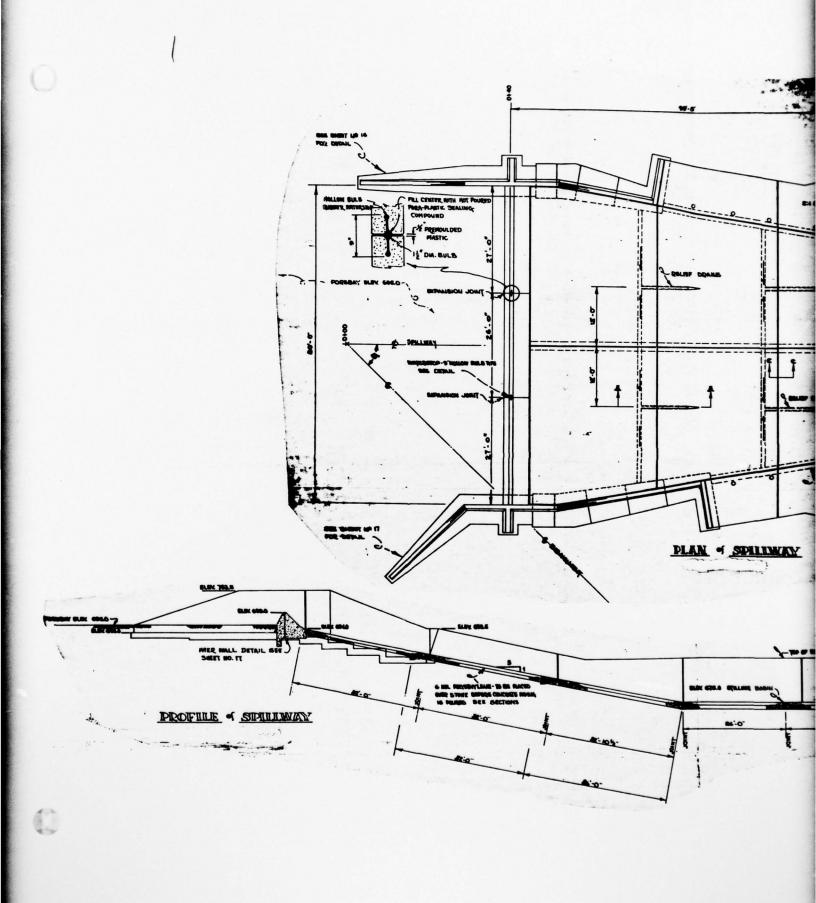
MOTE SUPPORT WALL AND SIDE WHILE

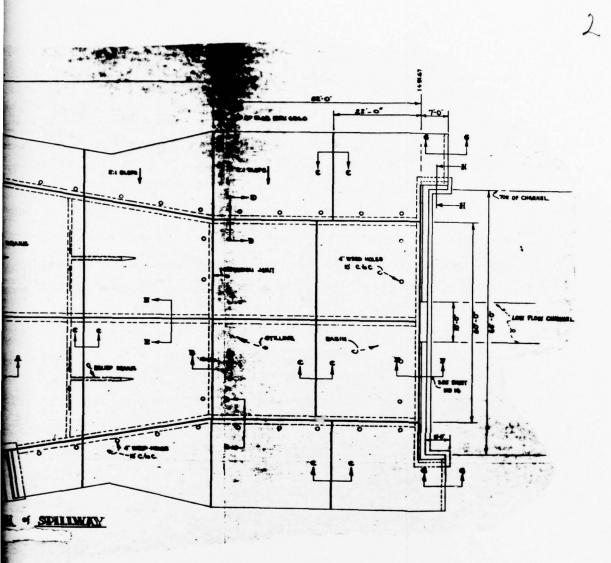
DETAILED SECTION OF CONTROL TOWER MINSI DAM

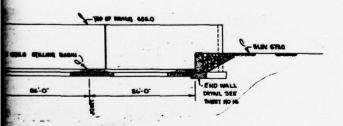
NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

DATA OBTAINED FROM PENNA. FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.13, DATED 4/19/68





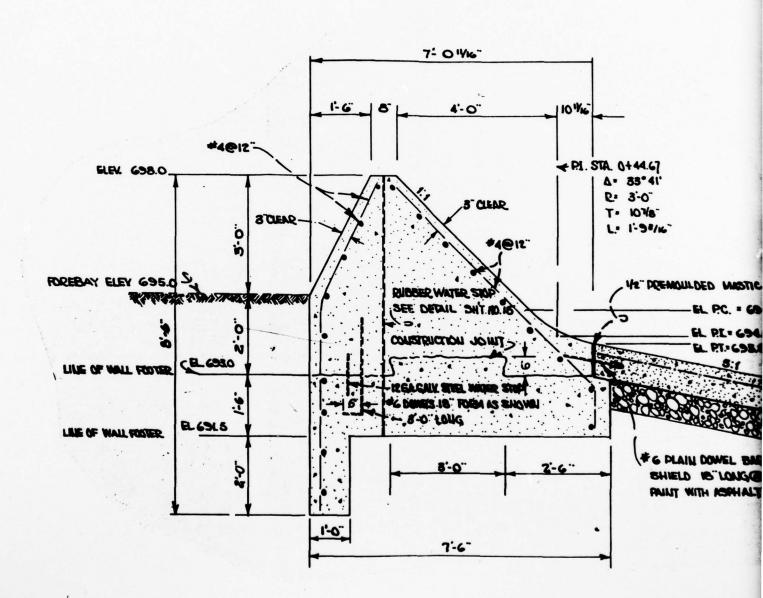


PLAN AND PROFILE OF EMERGENCY SPILLWAY MINSI DAM

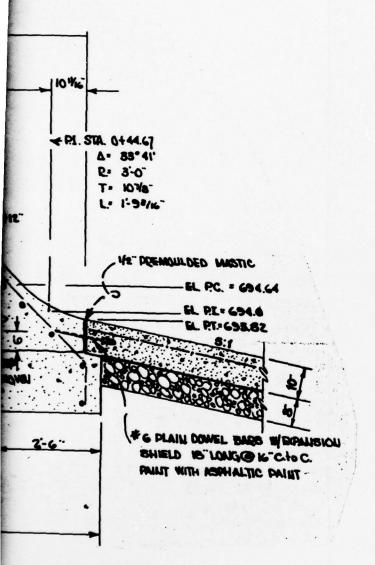
NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

DATA OBTAINED FROM PENNA. FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.15, DATED 4/10/68



2

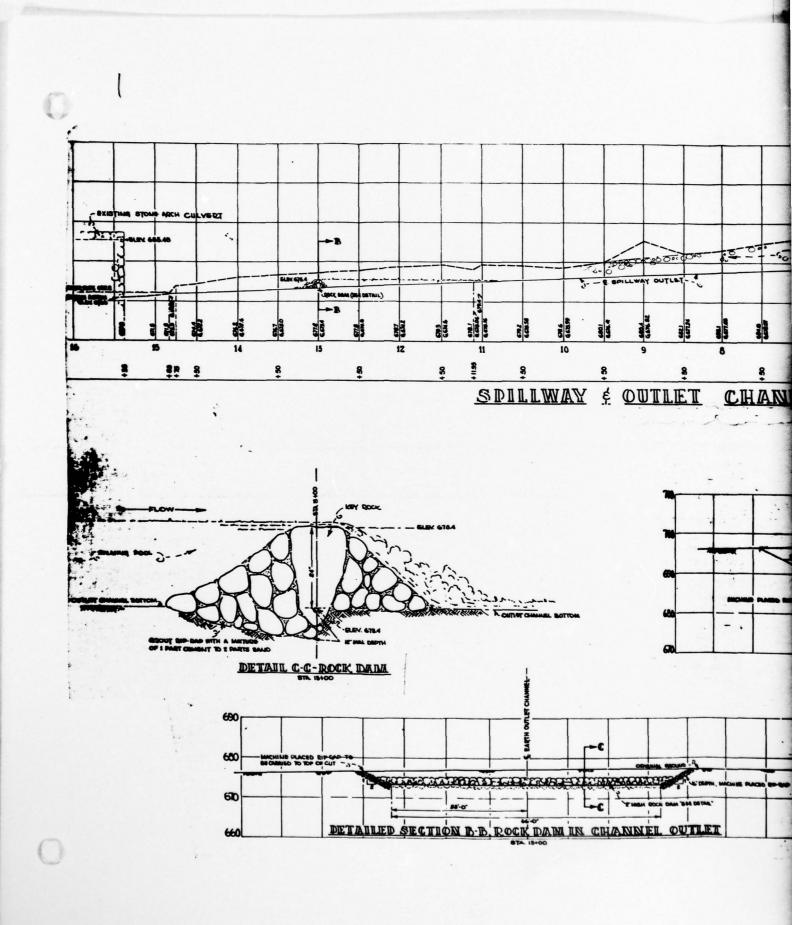


SPILLWAY CREST DETAILS MINSI DAM

NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

DATA OBTAINED FROM PENNA. FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.17, DATED 4/10/68



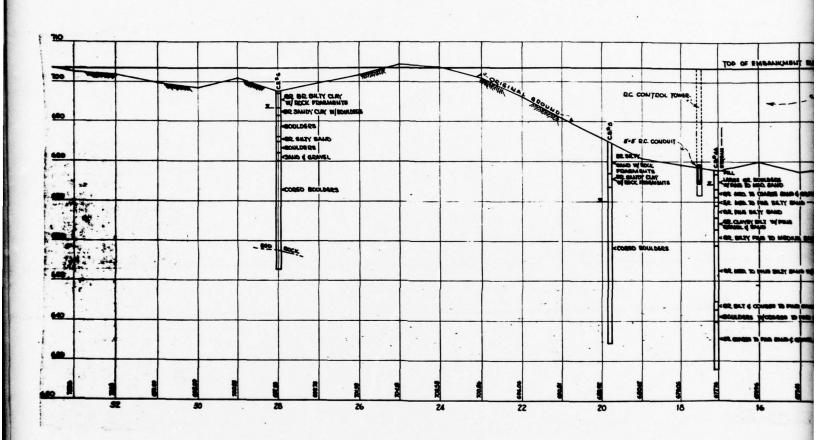
MIALLED SECTION AS OUTLET CHARNEL

SPILLWAY AND OUTLET CHANNEL PROFILE AND DETAILS MINS! DAM

NAT.I.D.NO.PA.00788

NORTHAMPTON COUNTY

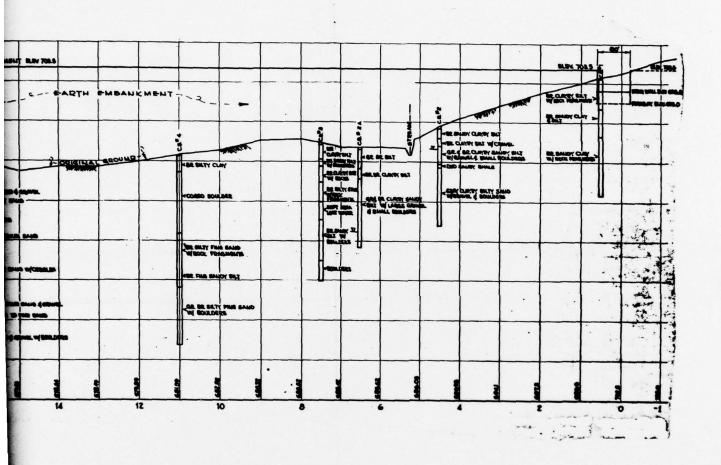
DATA OBTAINED FROM PENNA. FISH COMMISSION PROJECT NO. F.C.-160-L, SHEET NO.7 DATED 4/10/68



CORE	BORING	TABLE

HOLE	STATION	OFFSET	GROUND ELEY	APPROX WALE
NQ	SINTION	LT QT		
1	0 1 50	E	701.5	50'
2	4 + 50	6	668.9	50'
24	6 + 50	ē	683 . 1	50'
8	7 + 50	£	664 . 6	50'
4	11 + 50	•	681.6	50'
44	17 + 05	E	678.0	50'
5	69 + 80	ē	484.1°	50'
•	25 + 00	•	697.5	50'

LEGEND BROWN GRAY WITH BR GR W/ WED CB EC. CORE BORING BEINLOGOED CONCRETE GEONTO MYLES FEAST HTGAS



EMBANKMENT PROFILE AND CORE BORINGS MINSI DAM

NAT.I.D.NO.PA.00788

The state of the s

NORTHAMPTON COUNTY

DATA OBTAINED FROM PENNA. FISH COMMISION PROJECT NO. F.C-160-L, SHEET NO.6, DATED 4/10/68

APPENDIX

F

SITE GEOLOGY MINSI DAM

Minsi Dam is located in the Great Valley Section (adjacent to the Appalachian Mountain Section) of the Valley and Ridge Physiographic Province. As shown in Plate F-1, the bedrock underlying the dam site region is the Martinsburg Formation which consists predominantly of thick to thin bedded slates. Deposited over much of the bedrock, as is true for much of northeastern Pennsylvania, is a mantle of glacial drift. The regional bedrock structure is characterized by numerous northeast trending folds. A major regional northeast striking thrust fault (the Blue Mountain Decollement) is located approximately 1.75 miles north-northwest of the dam. Beneath the glacial cover, approximately 4,000 to 6,000 feet north-northwest of the dam, are two regional northeast trending folds with two similar folds located 3,000 to 4,000 feet to the southeast.

As indicated by data reviewed in the State files, the dam site area has a glacial cover consisting of 40 feet or more of silt and clay with interbedded lenses of silty sand and gravel and boulders overlying a quartzose slate (indicated as a shale sandstone in State files) bedrock. A northeastern strike and southeastern dip would most likely characterize the bedrock in the dam site area.

